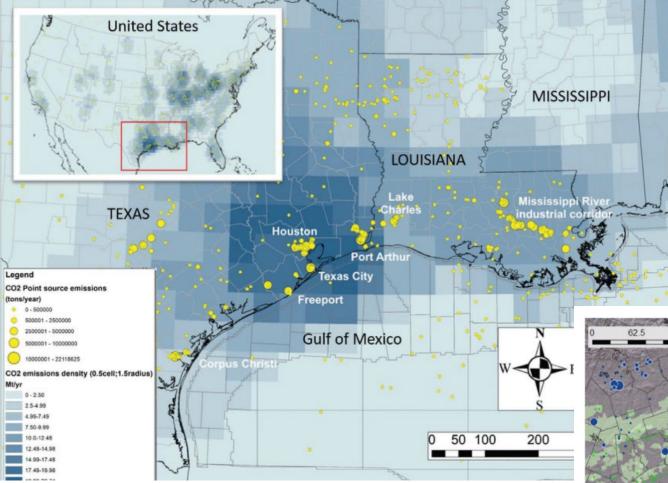
# **GoMCarb Publication Highlights**

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# GCCC, BEG, The University of Texas at Austin

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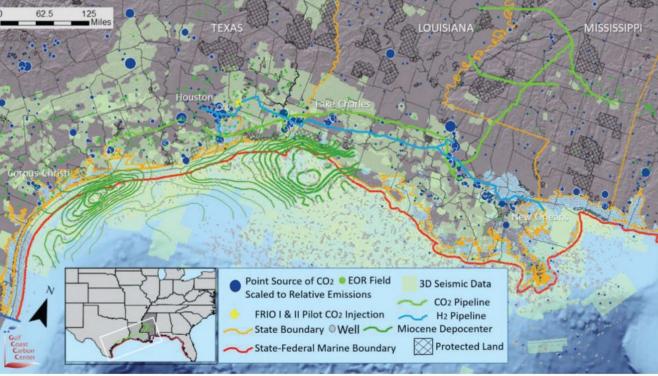


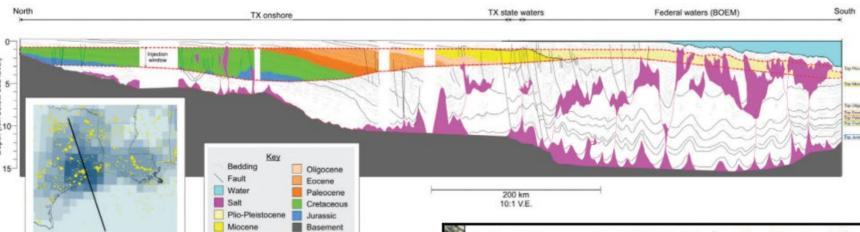
- <u>The Gulf Coast</u> of the United States hosts diverse power generation, refining, and petrochemical processing facilities, resulting in the <u>nation's largest volumetric</u> <u>concentration of industrial CO<sub>2</sub> emissions</u>, rivaled only by the Ohio River Valley.
- These emissions sources are <u>concentrated in specific</u> <u>industrial clusters that allow combining emissions</u> <u>streams to achieve economies of scale</u>.



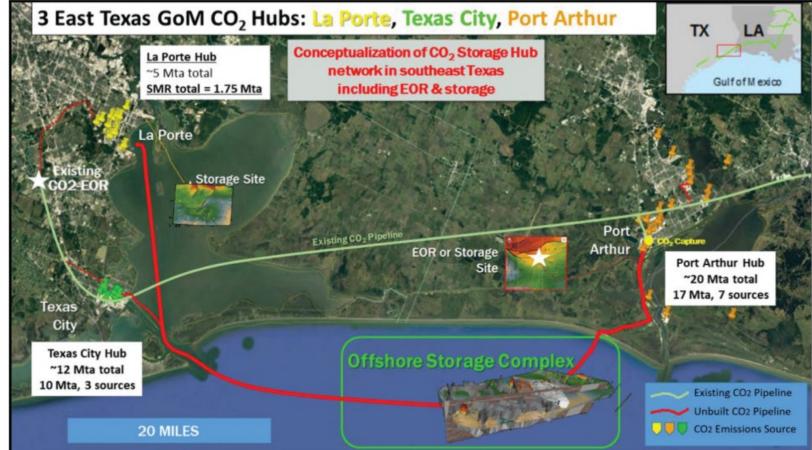
## on the Gulf Coast

T.A. Meckel, A.P. Bump, S.D. Hovorka 💿 and R.H. Trevino, The University of Texas at Austin, Austin, TX, USA





The region is currently undergoing globally significant industrial expansion and investment as a result of abundant and inexpensive regional unconventional natural gas availability, and is a growing exporter of liquefied natural gas (LNG).



- Offshore storage is particularly attractive, as it provides simplified land leasing models (single governmental land owner), proven reservoir quality, and presents fewer risks to both protected groundwater and populated areas.
- The region continues to evolve as an active carbon-handling hub, and is uniquely suited to justify additional investment in carbon capture, utilization, and storage (CCUS) technologies via a large-scale integrated project development.



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Assessing Impacts on Pressure Stabilization and Leasing Acreage for CO<sub>2</sub> Storage Utilizing Oil Migration Concepts

Melianna Ulfah<sup>a,\*</sup>, Seyyed Hosseini<sup>b</sup>, Susan Hovorka<sup>b</sup>, Alex Bump<sup>b</sup>, Sahar Bakhshian<sup>b</sup>, Dallas Dunlap<sup>b</sup>

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 <sup>b</sup> Gulf Coast Carbon Center, Bureau of Economic Geology, 10611 Exploration Way, Austin, TX 78758, United States

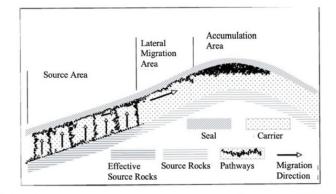


Fig. 1. Diagrammatic representation of migration pathways (modified from Zhang et al, 2006)





- If we inject CO<sub>2</sub> down to a syncline analogous to the carrier bed in the petroleum system – <u>how</u> would this injection mechanism impact storage capacity and plume shape, migration, and stabilization?
- To address this question, we built a reservoir model, based on seismic interpretation of Middle Miocene strata, offshore Galveston, Texas.
- Modeling investigated how far the CO<sub>2</sub> plume would migrate under two scenarios:
  - **1.** injecting  $CO_2$  at the base of the salt withdrawal basin (syncline scenario) and
  - 2. injecting  $CO_2$  at the base of the structural closure, similar to a common injection well location for EOR purposes (base scenario).

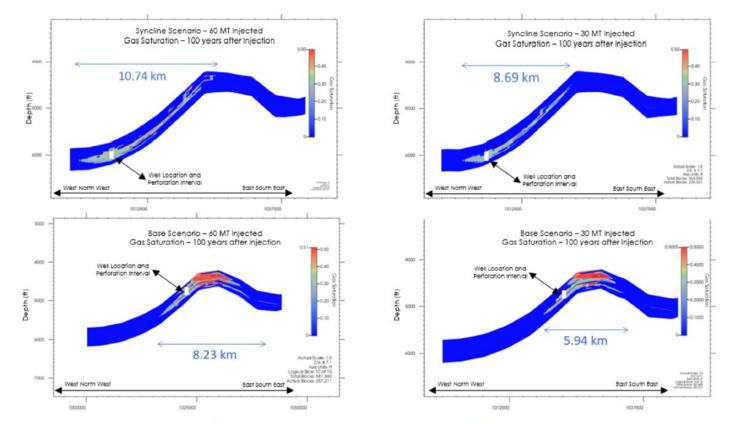
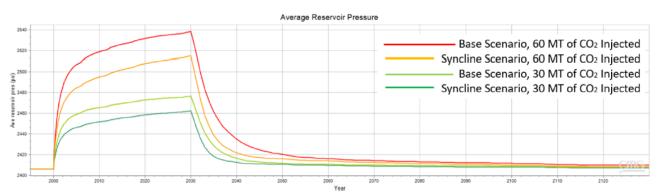


Fig. 14. Cross-section views of the plumes in all scenarios after 100 years after injection stops along with each of the lateral plume migration distances.



- The simulation shows that injecting the CO<sub>2</sub> into a syncline <u>limits the</u> <u>vertical migration of CO<sub>2</sub>, thus making</u> <u>synclinal injection more secure</u>.
- In the syncline scenario, the geological layer around the injection point is more heterogeneous than the layer in the base scenario; thus, the CO<sub>2</sub> tends to migrate laterally.
- Moreover, the simulation also shows that in the syncline scenario, <u>the</u> <u>times needed for the reservoir to</u> <u>reach its stabilized pressure after the</u> <u>end of injections are faster</u>.
- To summarize, CO<sub>2</sub> injection at the base of a syncline could provide additional storage, increase the safety of the project from the limited vertical plume migration, and expedite plume stabilization, which could result in the decrease of monitoring frequency as the project runs, thus lowering the operating cost of the project in the long run.

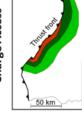
Fig. 18. Evolution of average reservoir pressure for all scenarios from the start of injection, 30 years of continuous injection, and 100 years after injection stops.



**Geologic Input Maps** 







Immature

Gas mature

Early oil mature Fully oil mature

Upper coastal plain

Lower coastal plain

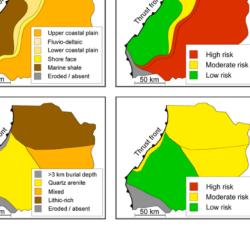
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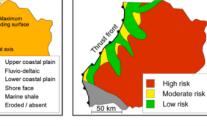
Shore face

Marine shale

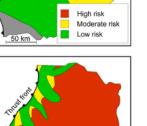
Froded / absent







50 km



High risk

Low risk

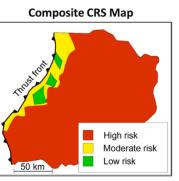
Hiah risk

Low risk

Moderate risk

Moderate risk

CRS Maps



 Rules of Addition

 Inputs
 Output

 All green
 Green

 Any yellow but no red
 Yellow

 Any red
 Red

ELSEVIE

# ELSEVIER

Common risk segment mapping: Streamlining exploration for carbon storage sites, with application to coastal Texas and Louisiana

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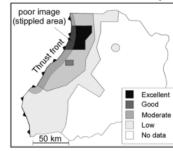
Alexander P. Bump<sup>\*</sup>, Susan D. Hovorka, Timothy A. Meckel Gulf Coast Carbon Center, Bureau of Economic Geology, Jackson School of GeoSciences, The University of Texas at Austin

- Large-scale deployment of Carbon Capture and Storage (CCS) will require a commensurately large number of sites.
- Efficient screening methods are needed to create investment assurance and focus efforts on the most promising sites.
- The problem is similar to petroleum exploration, for which there are welldeveloped (though seldom published) workflows, including <u>Common Risk</u> <u>Segment (CRS) mapping</u>.

#### Subsurface Data

#### Subsurface Data Density

Greenhous Gas Contro



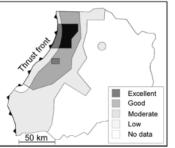
Subsurface Data Confidence

50 km

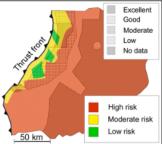
Well

3D seismic

2D seismic



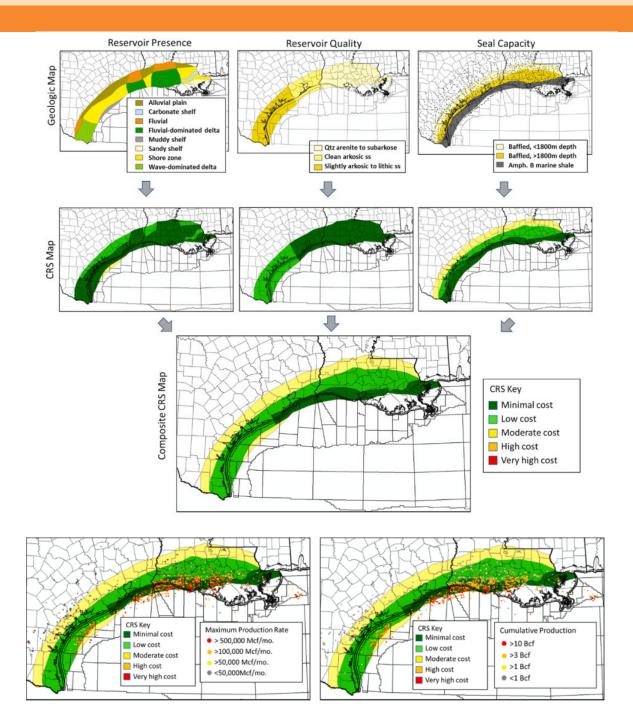




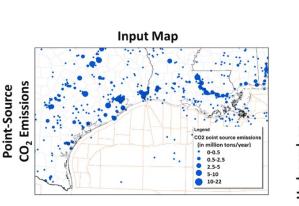


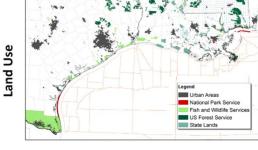


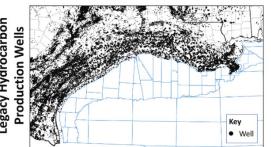
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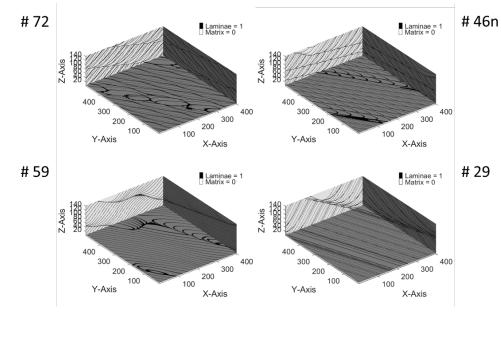
- In this paper, we adapt the CRS process to screening for CO<sub>2</sub> storage sites.
- Critically, we redefine the process in terms <u>of cost of</u> <u>characterization and development, rather than chance of</u> <u>success.</u>
- For illustration, we apply the process to the example of the Lower Miocene on the Texas and Louisiana Gulf Coast.
- We show that the predictions are consistent with historic hydrocarbon production volumes and rates.
- The result <u>highlights sweet spots and identifies critical risks</u>, suggesting a focus for further data collection and analysis.
- The method developed here can be applied to <u>both surface</u> <u>and subsurface factors</u> anywhere that there is interest in geologic storage of CO<sub>2</sub>.







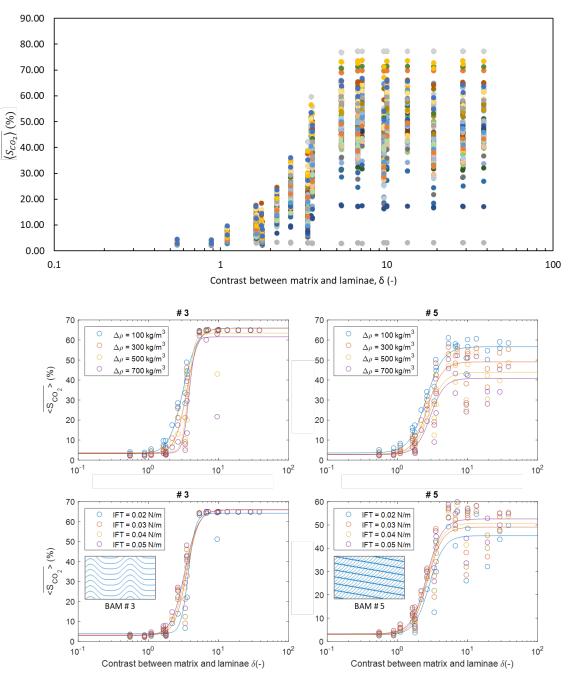
# Scientific reports OPEN Effects of grain size and small-scale bedform architecture on CO2 saturation from buoyancy-driven flow Halun Ni®, Sahar Bakhshian & T.A. Meckel



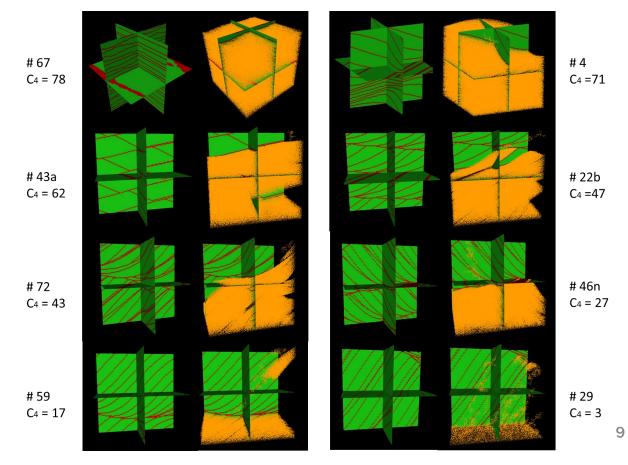


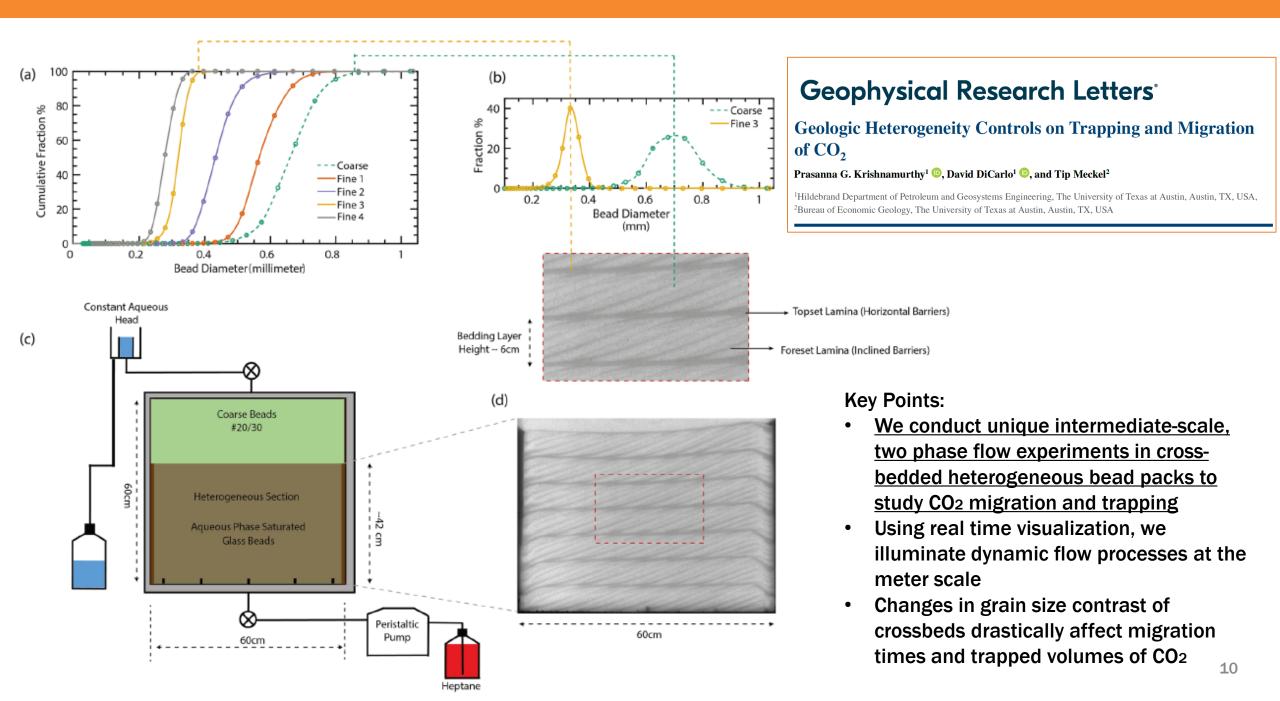
	1		SAND							
	SORTING	COARSE		MEDIUM		FINE		VERY FINE		COARSE
	So	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER	LOWER	UPPER
Extremely Well Sorted	1.05	EWUCSa		EWUMSa		EWUFSa	0	EWUVFSa	0	EWUCSI
Very Well Sorted	1.15	VWUCSa		VWUMSa		VWUFSa	$\bigcirc$	VWUVFSa	$\bigcirc$	vwucsi
Well Sorted	1.30	WUCSa		WUMSa		WUFSa	$\bigcirc$	WUVFSa	0	wucsi
Moderately Sorted	1.70	MUCSa		MUMSa		MUFSa		MUVFSa	0	MUCSI
Poorly Sorted	2.35	PUCSa	Ø,	PUMSa		PUFSa	0	PUVFSa	0	PUCSI
Very Poorly Sorted	4.20	VPUCSa		VPUMSa		VPUFSa		VPUVFSa		VPUCSI
MEDIAN DIAMETER $\cdot$ $d_{50}$ (mm)		<b>♦</b> 0.840	0.590	0.420	0.297	0.210	0.149	0.105	0.074	0.053

- Small-scale (mm-dm scale) heterogeneity has been shown to significantly impact CO<sub>2</sub> migration and trapping.
- <u>Realistic simulation domains are constructed by varying two</u> <u>important aspects of small-scale geologic heterogeneity</u>: <u>sedimentary bedform architecture</u> and <u>grain size contrast</u> between the matrix and the laminae facies.
- Buoyancy- driven flow simulation runs cover 59 bedform architecture and 40 grain size contrast cases.

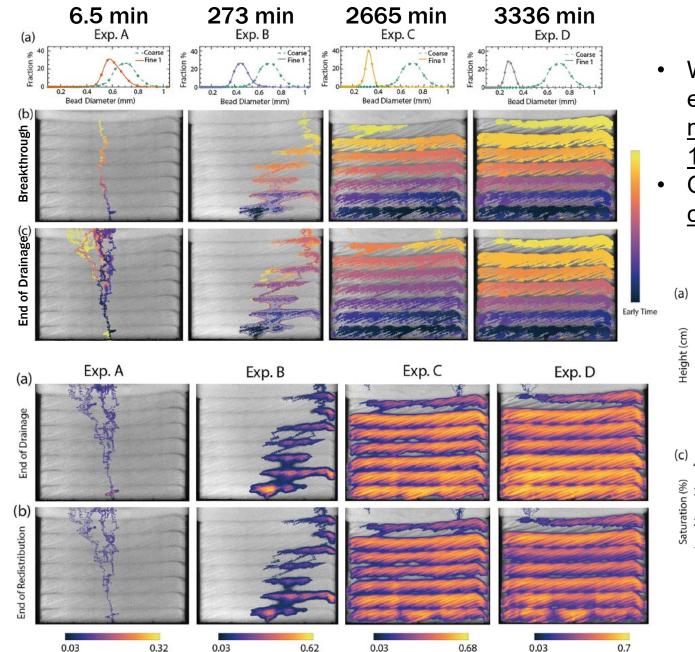


- Simulation results show that the <u>domain effective CO<sub>2</sub> saturation is</u> <u>strongly affected by both grain size and bedform architecture</u>.
- Differences in <u>bedform architecture</u> can impact how CO<sub>2</sub> saturation values respond to other variables such as <u>grain sorting</u> and <u>fluid</u> <u>properties</u>.
- The value of this study is to <u>provide a comprehensive simulation</u> <u>dataset</u>, upon which <u>prediction models</u> can be built for upscaling purposes in field-scale simulations.

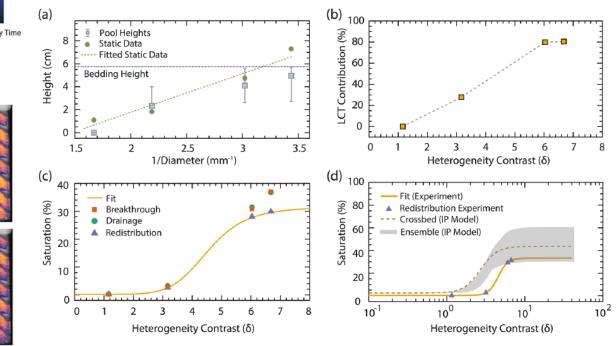




#### **Breakthrough time**



- We show that subtle changes in rock properties, especially the grain size contrast, <u>can slow down</u> <u>migration speeds and increase trapped volumes by 10–</u> <u>100 times</u>.
- Our results also show that <u>heterogeneities can</u> <u>contribute up to 80% of the total storage capacity</u>.



## Original Research Article



# Major CO<sub>2</sub> blowouts from offshore wells are strongly attenuated in water deeper than 50 m

**Curtis M. Oldenburg D and Lehua Pan**, Energy Geosciences Division, Lawrence Berkeley National Laboratory, Berkeley, CA, USA

- Growing interest in offshore geologic carbon sequestration (GCS) motivates evaluation of the <u>consequences of subsea CO<sub>2</sub> well blowouts</u>.
- <u>We have simulated a hypothetical major CO<sub>2</sub> well</u> blowout in shallow water of the Texas Gulf Coast.
- We use a coupled reservoir-well model (T2Well) to simulate the subsea blowout flow rate for input to an integral model (TAMOC) for modeling CO<sub>2</sub> transport in the water column. Bubble sizes are estimated for the blowout scenario for input to TAMOC.

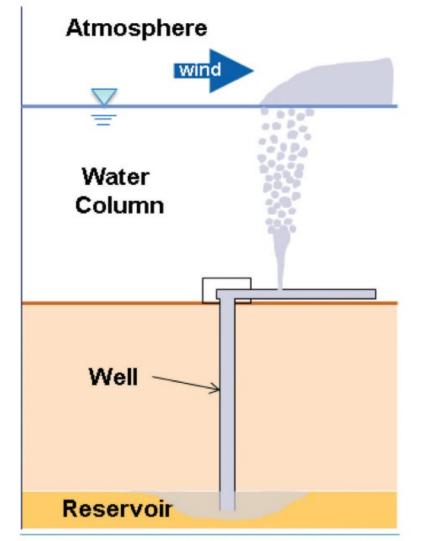


Figure 1. Conceptual model of an offshore CO<sub>2</sub> well with blowout near the wellhead showing the reservoir, well, short pipe segment, water column, and atmospheric regions.



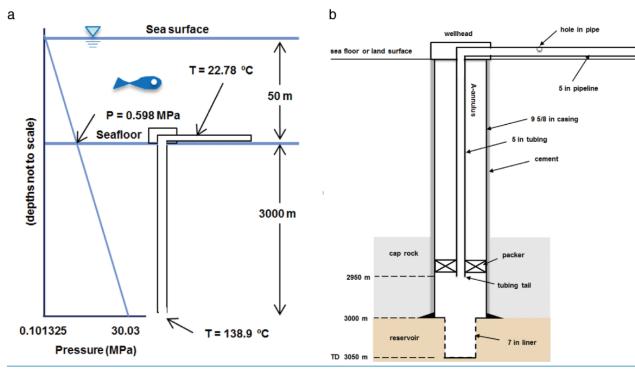
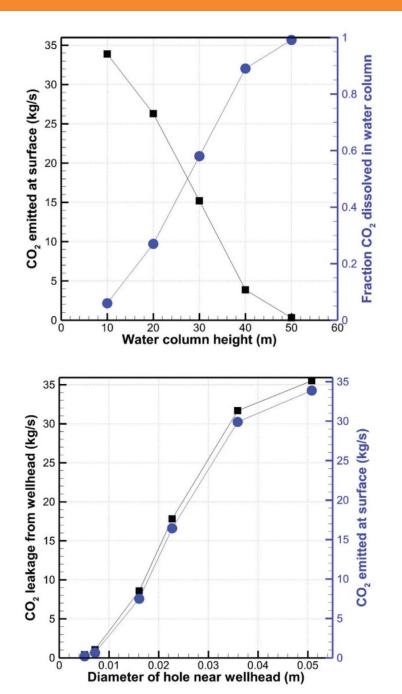


Figure 3. (a) Sketch of pressure, temperature, and depth conditions for the 50-m-deep offshore well, and (b) reservoir and well system domain used in the T2Well blowout simulation.

- Results suggest that <u>a major CO<sub>2</sub> blowout in ≥50 m of water will be almost</u> <u>entirely attenuated by the water column due to CO<sub>2</sub> dissolution into</u> <u>seawater during upward rise</u>.
- In contrast, the same blowout in 10 m of water will hardly be attenuated at all.
- Results also show that the size of the orifice of the leak strongly controls the CO<sub>2</sub> blowout rate.





### Modeling and Analysis



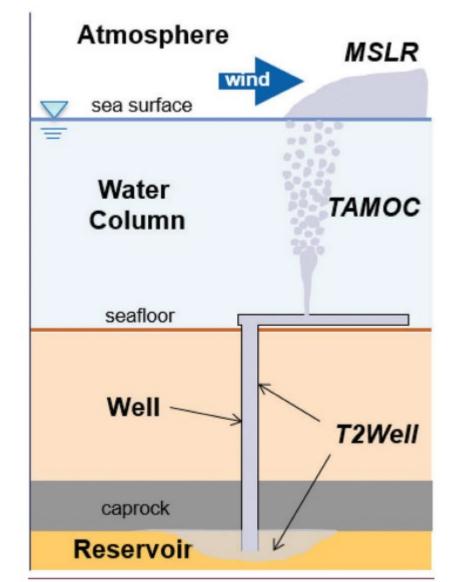
# Downwind dispersion of CO<sub>2</sub> from a major subsea blowout in shallow offshore waters

Curtis M. Oldenburg D and Yingqi Zhang, Lawrence Berkeley National Laboratory, Berkeley, CA, USA

- In the context of risk assessment of human health and safety, we have used previously simulated coupled wellreservoir and water column model results <u>as a source</u> <u>term for dense gas dispersion of CO<sub>2</sub> above the sea</u> <u>surface.</u>
- <u>The models are linked together by one-way coupling</u>, that is, output of one model is used as input to the next model.
- <u>These first-of-their-kind coupled flow results are</u> <u>applicable to assessing the hazard of CO<sub>2</sub> to people at</u> <u>and downwind of the sea surface location of emission.</u>

Economic

Geology



14

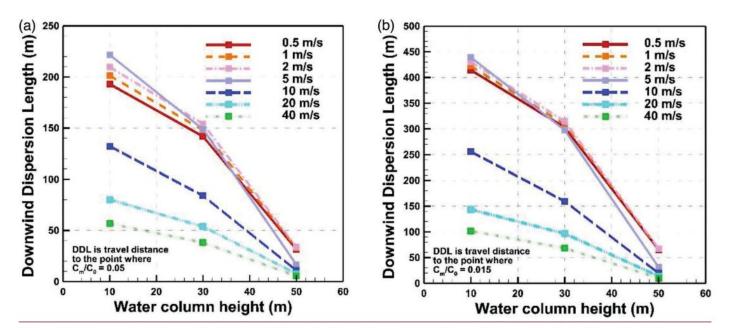


Figure 3. Downwind dispersion length (DDL) for the subsea  $CO_2$  blowout scenarios for different water column heights (different surface leakage rates) and wind speeds for two different critical concentrations: (a)  $C_m/C_0 = 0.05$ ; (b)  $C_m/C_0 = 0.015$  (note the different y-axis scales)

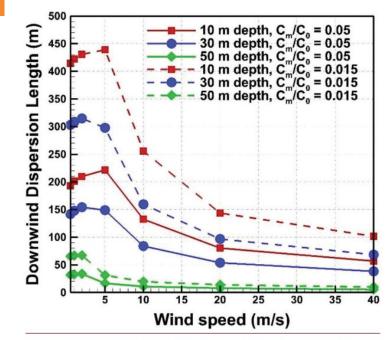
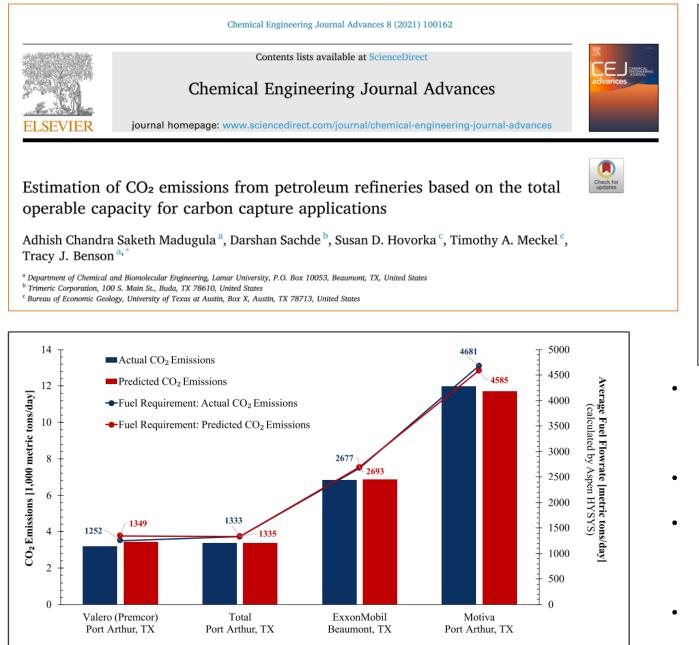
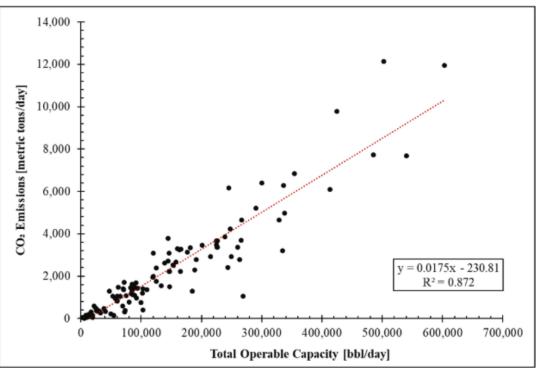


Figure 4. DDL as a function of windspeed for three different water column depths and two different critical concentrations. The plot shows that a maximum DDL occurs for windspeeds of 2–5 m/s depending on the case

- <u>Hazard is quantified by plotting the downwind dispersion length (DDL)</u>, which we define in the study as the distances from the emission source to the point at which the emitted CO<sub>2</sub> has been diluted to 5% and 1.5% in air by volume.
- Results suggest that <u>large-scale blowouts in shallow water (10 m) may cause hazardous CO<sub>2</sub> plumes extending on the order of several hundred meters downwind.
  </u>
- Details of the modeling show <u>DDL has a maximum for windspeed (at an elevation of 10 m) of approximately 5 m/s</u>, with smaller DDL for both weaker and stronger winds.
- This is explained by the fact that wind favors transport but also causes dispersion; therefore there is a certain wind speed that maximizes DDL.







- <u>Petroleum refineries, in particular, produce several streams that are</u> <u>CO<sub>2</sub>-rich</u>, including fluidized catalytic cracking, steam methane reforming, and natural gas combustion processes that generate heat for re- finery operations.
- Of these, stationary combustion processes account for nearly twothirds of all CO<sub>2</sub> generated within a refinery.
- In this work, a regression analysis was performed to correlate the size and power requirements for the combined capture, compression, and dehydration process dependent upon a refinery's operating capacity.
- <u>Refinery capacity and CO<sub>2</sub> generation data from 128 U.S. refineries</u> were normalized, and a linear regression model was developed.

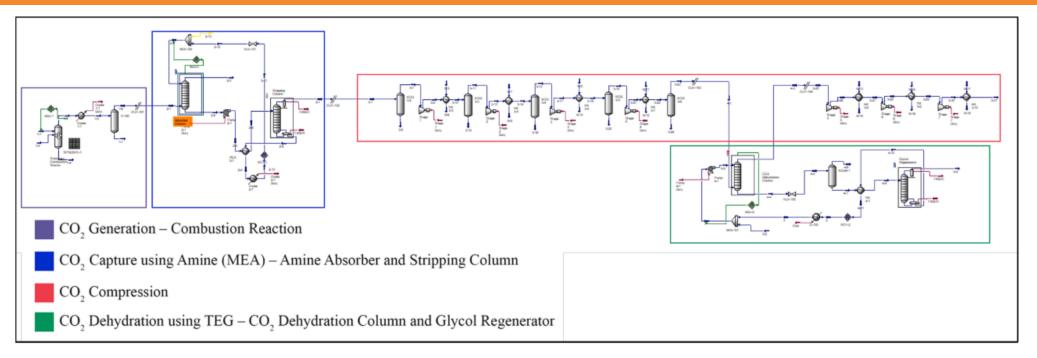
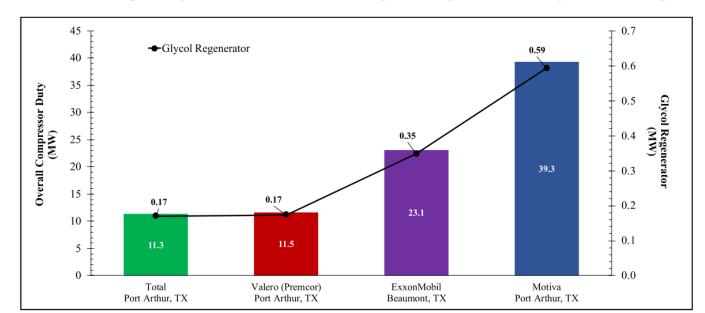


Fig. 2. Aspen HYSYS Simulation of the capture, compression, and dehydration of flue gas CO<sub>2</sub> from stationary combustion source



- <u>A capture, compression, and dehydration</u> process model was developed using Aspen HYSYS for delivery of CO<sub>2</sub> (10–15 wt. % in steam) to pipeline specifications (500 ppm H<sub>2</sub>O, 15.2 MPa).
- <u>Predicted CO<sub>2</sub> emissions were 0.1 to 7.7 %</u> of actual emissions, depending on whether a refinery had a low, medium, or high carbon emission/capacity ratio.